



Institute of Aeronautics and Applied Mechanics

# Finite element method 2 (FEM2)

Error estimation in a finite element

10.2021

## A - POSTERIORI ERROR APPROXIMATION

VECTOR OF THE AVERAGE STRESS AT NODE  $i$  :

$$\{\sigma\}_i^{ave} = \frac{\sum_{e=1}^k \{\sigma\}_i^e}{k}$$

where :

$k$  - number of elements adjacent to node  $i$

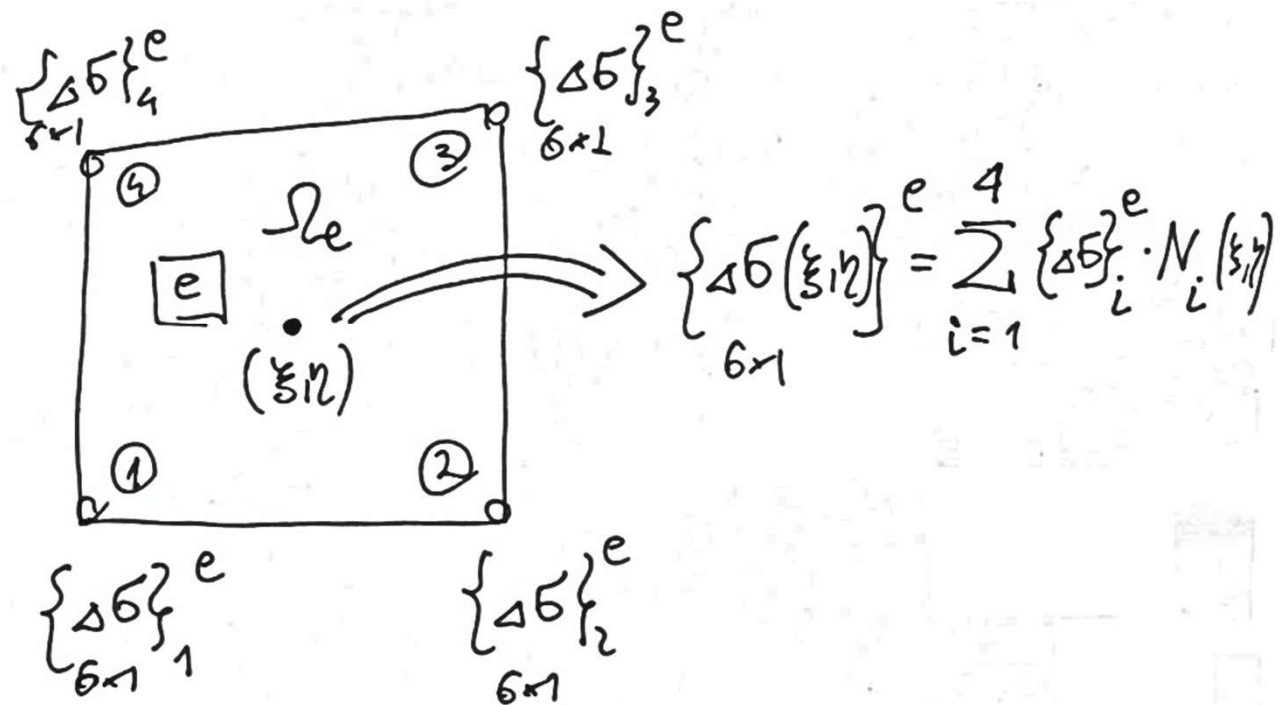
$e$  - element number

$$\{\sigma\}_i^e = \begin{Bmatrix} \sigma_x \\ \sigma_y \\ \sigma_z \\ \tau_{xy} \\ \tau_{yz} \\ \tau_{zx} \end{Bmatrix}_i^e$$

THE STRESS ERROR IN ELEMENT  $e$  AT NODE  $i$  :

$$\{\Delta \sigma\}_i^e = \{\sigma\}_i^e - \{\sigma\}_i^{ave}$$

$6 \times 1$                        $6 \times 1$



The maximum absolute value of any stress component :

$$\max \left( \left\{ \Delta \sigma \right\}_i^e \right)_{6 \times 1} \quad (\text{SDSG-IN ANSYS})$$

Strain energy in a finite element :

$$U_e = \frac{1}{2} \int_{\Omega_e} [B]^e \cdot \left\{ \varepsilon \right\}^e d\Omega_e = \frac{1}{2} \int_{\Omega_e} [B]^e [D]^{-1} \left\{ \sigma \right\}^e d\Omega_e$$

↑  
Inverse constitutive matrix

strain energy density in a finite element

$$u_e = \frac{U_e}{\int_{\Omega_e} d\Omega_e} \quad (\text{SENDELAS-IN ANSYS})$$

Total strain energy for the entire model:

$$U = \sum_{e=1}^{NOE} U_e$$

Strain energy error in a finite element:

$$\Delta U_e = \frac{1}{2} \int_{S_e} [B]_{1 \times 6}^e [D]_{6 \times 6}^{-1} \cdot \{\Delta \delta\}_{6 \times 1}^e dS_e \quad (\text{SERP-IN ANSYS})$$

Total strain energy error in the entire model:

$$\Delta U = \sum_{e=1}^{NOE} \Delta U_e$$

The normalized energy error (for the entire model) is calculated as:

$$S = 100 \cdot \sqrt{\frac{\Delta U}{\Delta U + U}} \quad (\text{SERP IN ANSYS})$$

The procedure of mesh refining:

$\Delta U_e = \text{const}$  for all FEs - "error equilibration"

$S < S_0$  for the entire model

$S_0$  - allowable value of  $S$ .

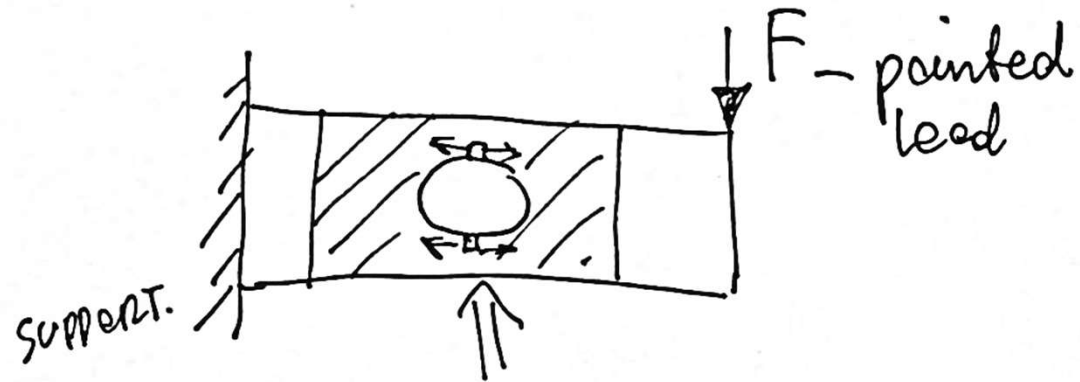
1°) Adaptive meshing - to correct mesh until:

$$\frac{\Delta U_e - \frac{\Delta U}{NOE}}{\frac{\Delta U}{NOE}} < \Delta U_0$$

↑ allowable value.

and  $S < S_0$

## 2°) Selective adaptive meshing



### TYPES OF REFINEMENT:

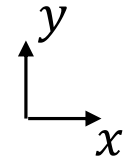
$h$  - size decrease

$p$  - polynomial order in shape functions

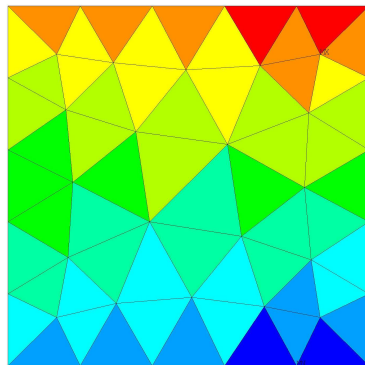
$r$  - nodes rearrangement

$h_p$  - combination of "h" and "p"

# Normal stress in x direction (SX)

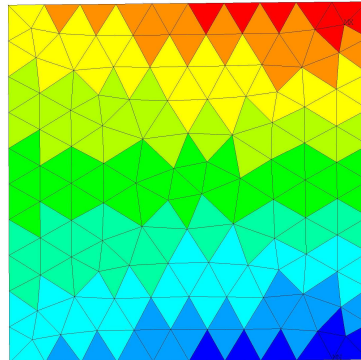


CST, 4mm  
(free mesh)



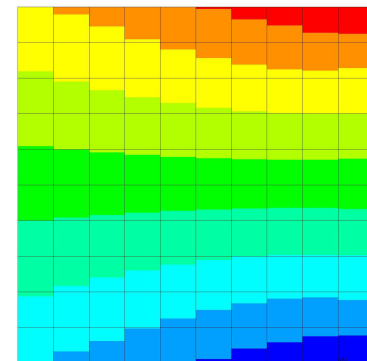
SMN = 29.9391  
SMX = 50.0735

CST, 2mm  
(free mesh)



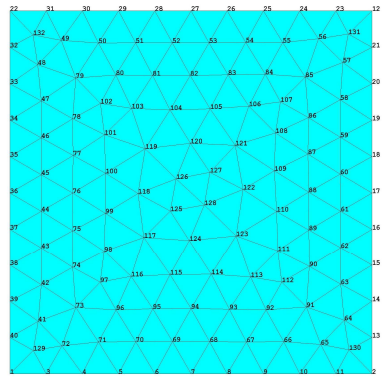
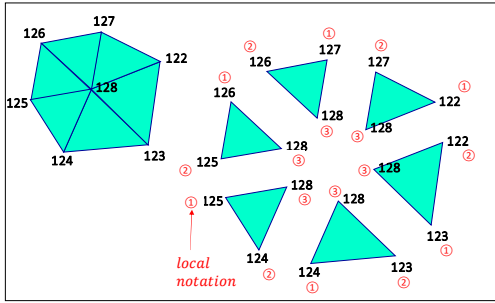
SMN = 31.3547  
SMX = 48.657

QUAD-4node, 2mm  
(mapped mesh)



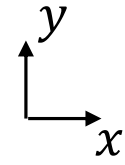
SMN = 31.2497  
SMX = 48.819

### FEM 1. HOMEWORK 1

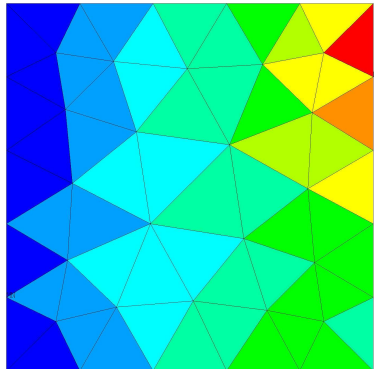





# Normal stress in y direction (SY)

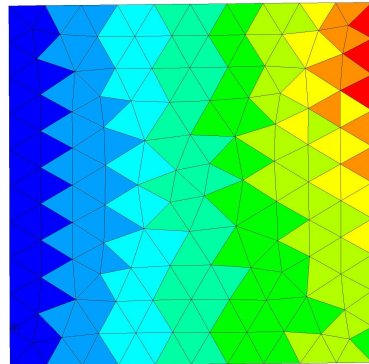


CST, 4mm



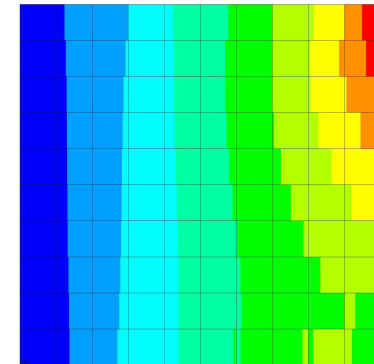
SMN =22.4161  
SMX =31.2216

CST, 2mm



SMN =22.4077  
SMX =30.4297

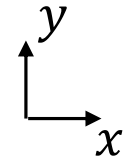
QUAD-4node, 2mm



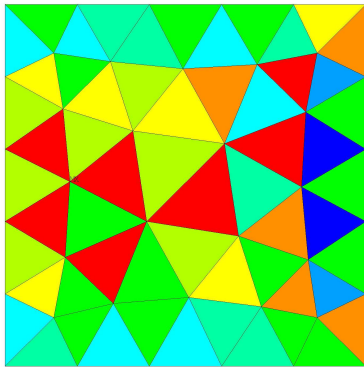
SMN =22.3724  
SMX =30.5656

(MPa)

# Shear stress (SXY)

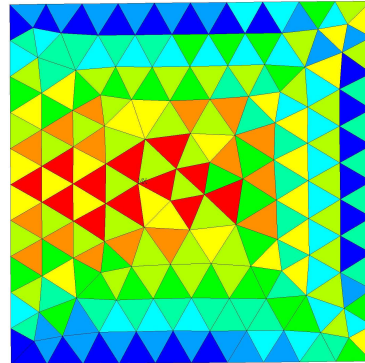


CST, 4mm



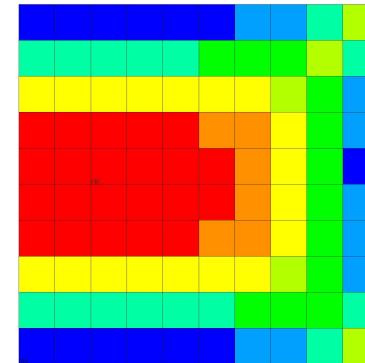
SMN =20.9712  
SMX =22.9216

CST, 2mm



SMN =21.4276  
SMX =22.7416

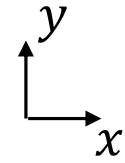
QUAD-4node, 2mm



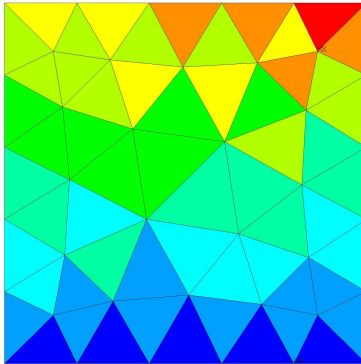
SMN =21.553  
SMX =22.4885

(MPa)

# Von Mises stress (SEQV)

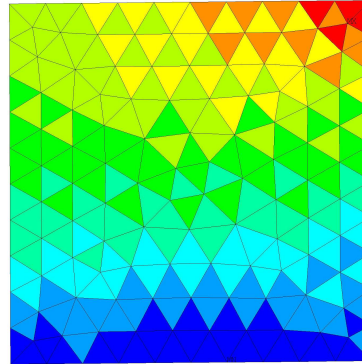


CST, 4mm



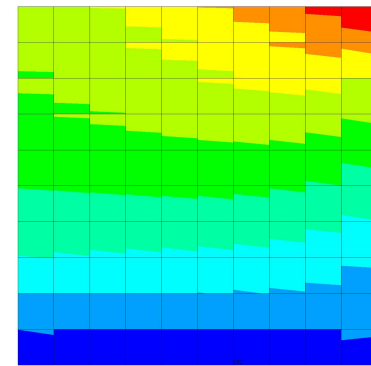
SMN =47.474  
SMX =58.2418

CST, 2mm



SMN =47.9007  
SMX =57.2223

QUAD-4node, 2mm



SMN =47.9151  
SMX =57.431

(MPa)

# Elastic strain energy (SENE)

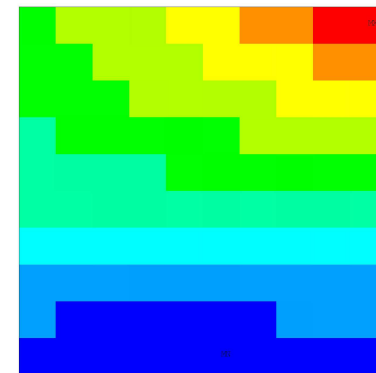
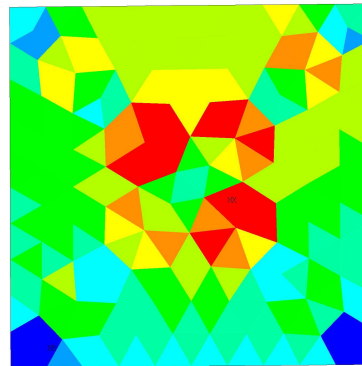
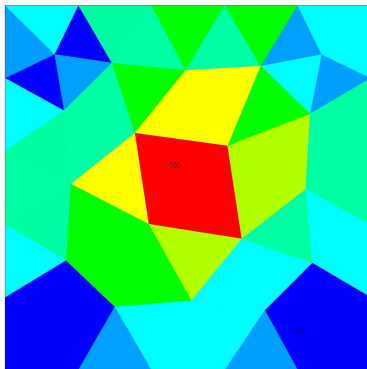
$$U_e = \frac{1}{2} \int_{\Omega_e} [\varepsilon] \{\sigma\} d\Omega_e \quad (\text{Nmm})$$

CST, 4mm

CST, 2mm

QUAD-4node, 2mm

(SENE)

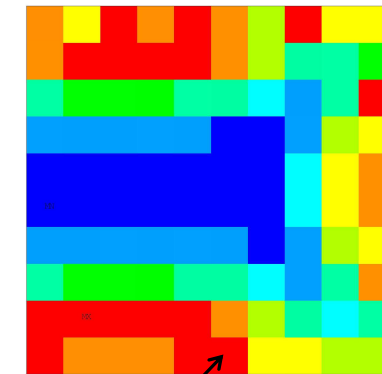
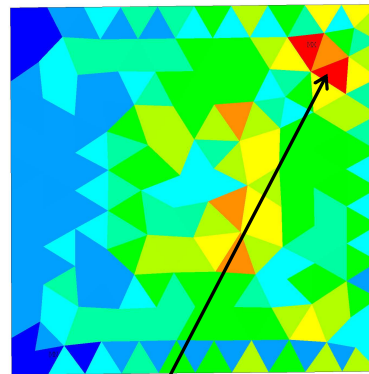
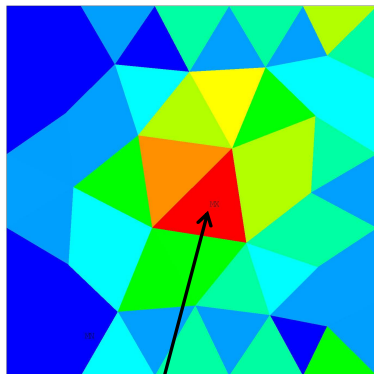


SMN = .029352  
SMX = .093964

SMN = .007026  
SMX = .019023

SMN = .024947  
SMX = .035708

Error (SERR)



SMN = .944E-05  
SMX = .155E-03  
(SEPC= 4.06%)

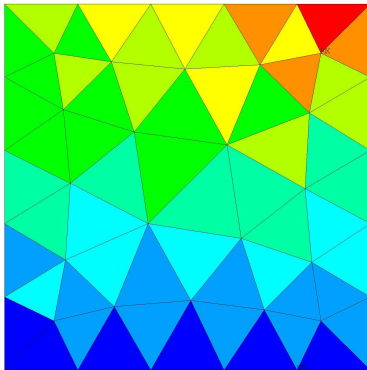
SMN = .434E-06  
SMX = .624E-05  
(SEPC= 1.92%)

SMN = .309E-07  
SMX = .945E-06  
(SEPC= 0.51%)

# Elastic strain energy density (SENDELAS)

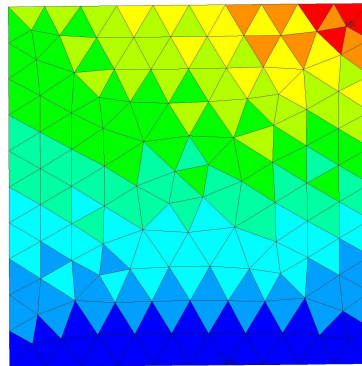
$$u_e = \frac{U_e}{\int_{\Omega_e} d\Omega_e}$$

CST, 4mm



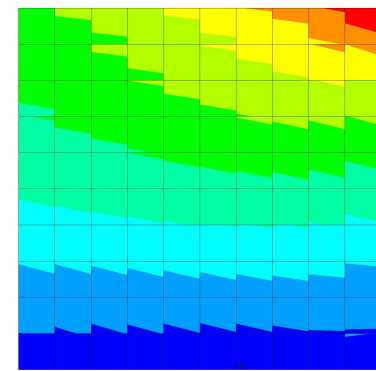
SMN = .005946  
SMX = .009429

CST, 2mm



SMN = .006126  
SMX = .009121

QUAD-4node, 2mm

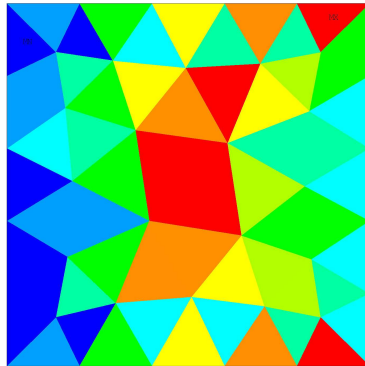


SMN = .006113  
SMX = .009243

(Nmm/mm<sup>3</sup>)

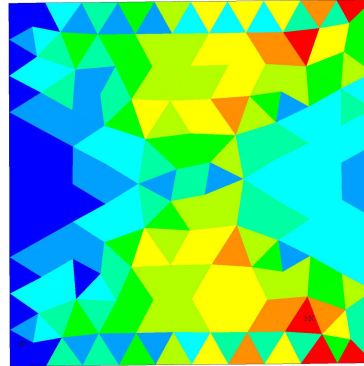
# Maximum absolute value of error of any stress component (SDSG)

CST, 4mm



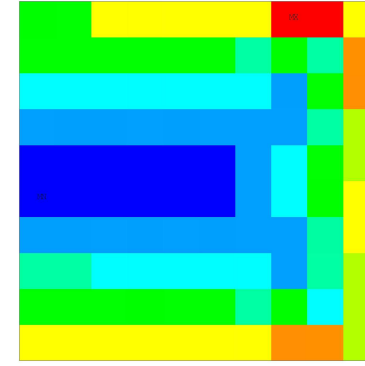
SMN =1.07305  
SMX =3.37362

CST, 2mm



SMN =.490022  
SMX =1.61018

QUAD-4node, 2mm



SMN =.045321  
SMX =.338378

(MPa)